STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN FOR THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN IN THE REPUBLIC OF NAMIBIA

Japan International Cooperation Agency Pacific Consultants International

BOREHOLE FINAL REPORT

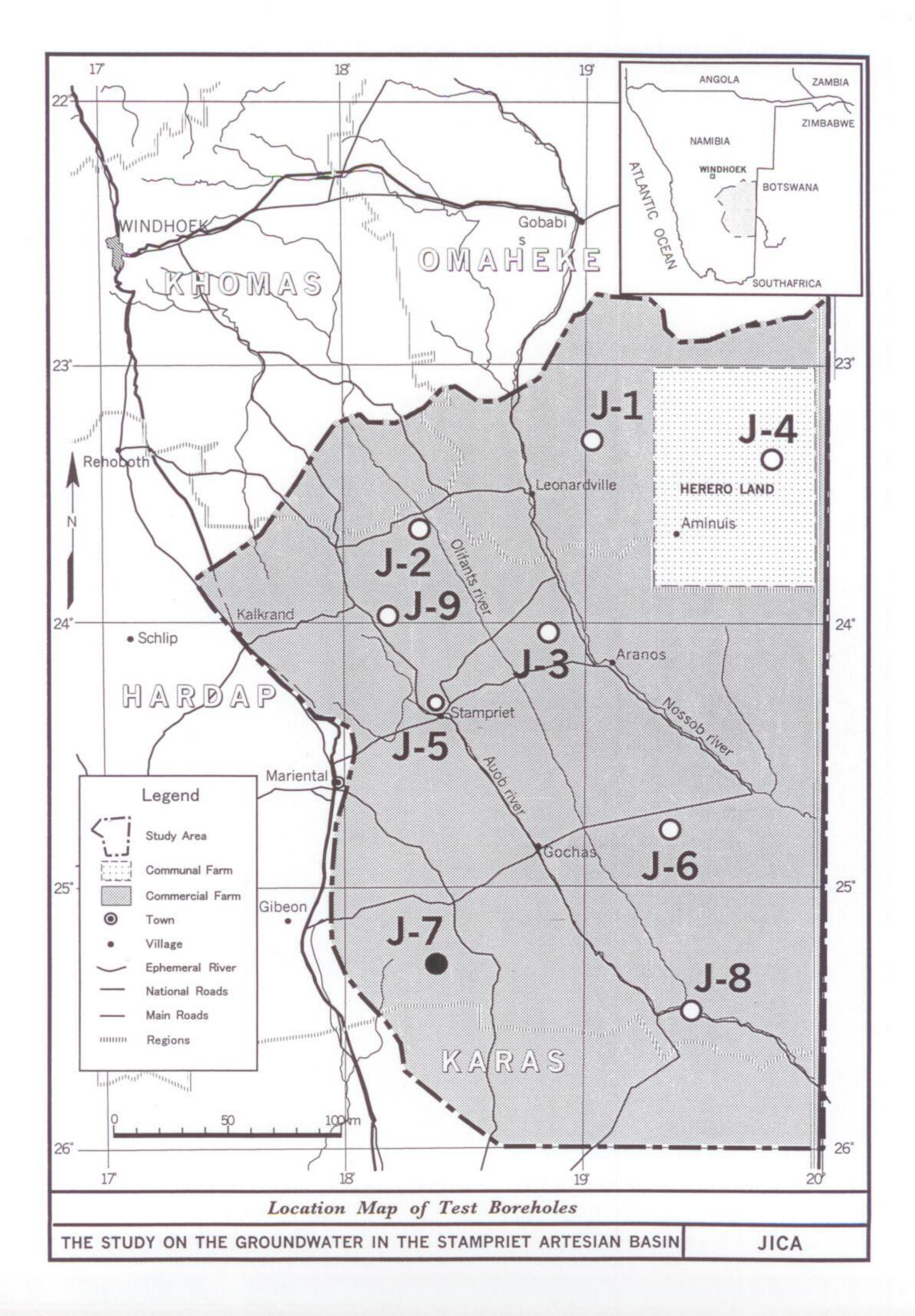
Borehole J7-N (WW 39853) Jakkalsdraai R 228

METZGER PM DRILLING

P.O.Box 11733 Windhoek Namibia

Windhoek

October 2000



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1. Geological Borehole Log



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

Farm Jakkalsdraai	WW 39853
Jica Reference: J 7 N	S 25, 29107 °
Date completed: 5 August 2000	E 18, 41756 °
	Collar elev.: 1144 mamsl

GEOLOGICAL	BOREHOLE LOG	
ULULUUICAL	DOVEHOLE FOR	

Depth below surface (m)	Section (m)	Lithology	Stratigraphy
0-7	7	Light brownish grey calcrete, slightly karsted near surface.	
7 – 14	7	Calcretized gravel and conglomerate. Calcrete matrix white to light grey.	
14 - 26	12	Pale reddish brown calcretized sand with horizons of gravelly calcretized conglomerate.	
26 - 27	1	Pinkish massive calcrete.	1
27 – 29	2	Pinkish unsorted sandstone with scattered quartz granules. Calcareous & porous. Aquifer.	KALAHAR
29 - 32	3	Pale grey to pale brownish conglomerate cemented with calcrete.	
32 -34	2	Poorly sorted, partially consolidated conglomerate in a grey sandstone-matrix. Granules and pebbles well rounded. Porous. Aquifer.	
34 - 44	10	Unsorted, non-calcareous sandstone, to moderately calcareous in places, slightly porous with silcretes horizons. Pale reddish brown.	
44 - 49	5	Conglomerate in a pinkish calcrete matrix.	
49 - 53	4	Pale yellowish fine to medium grained micaceous sandstone (muscovite & biotite) laminated.	
53 - 57		Pale yellowish fine to medium grained laminated micaceous sandstone, interbedded with pale yellowish orange shale. Aquitard. Fe oxidation on laminae.	
57 - 62	5	Pale yellowish brown well sorted medium grained non- calcareous sandstone. Quartz grains subrounded.	RIETMONE
62 - 65	3	Moderately calcareous, porous medium grained pale yellowish brown sandstone. Minor muscovite.	
65 - 68.5	3.5	Moderately calcareous calcareous, porous medium grained pale yellowish brown sandstone , interbedded with brownish grey sandstone.	
68.5 - 75	6.5	Fine to medium grained light grey sandstone. Grains well rounded. Moderately porous. Scattered dark grey shaly clasts.	AUOB
75 - 81	6	Laminated grey fine-grained sandstone. Biotite on laminations, increasing with depth.	A 5
81 - 89	8	Grey laminated siltstone. Abundant biotite on laminae.	
89 - 93	4	Dark grey micaceous shale with minor siltstone horizons. Jointing with calcite veins.	

1

93 - 99	6	Grey laminated siltstone/shale with minor biotite.	
99 - 109	10	Inter-layered sandstone - siltstone - shale. Shale grey to dark grey.	AUOB A 4
109 - 127	18	Shale, light grey turning to grey and dark grey with increasing depth.	
127 - 133	6	White to very pale grey coarse well sorted sandstone, porous. Quartz grains sub-rounded. Moderately calcareous at 131 – 133 m. Aquifer.	
133 - 138	5	Grey to pale grey medium grained sandstone with scattered shale clasts. Moderately porous. Aquifer.	AUOB A 3
138 - 154,5	16,5	Pale grey fine grained laminated micaceous sandstone with poor porosity.	
154,5 - 160,5	6	Grey to dark grey micaceous (biotite) fine to very fine sandstone. Very thin dark grey shale at 154,5.	AUOB
160,5 - 166	5,5	Grey sandstone, fine grained with black / dark grey clasts of coal (?). Muscovite associated with coal.	A 1
166 - 175	9	Laminated grey siltstone / shale.	UPPER MUKOROB
175 - 228	53	Grey to dark grey shale. Bituminous at 204 – 209 m. Dropstones at 216 m.	LOWER MUKOROB
228 - 234.5	6,5	Fine grained well sorted light grey sandstone. Slightly porous. Friable. Sandstone is very fine grained at 234 m. Aquifer.	
234.5 - 236	1,5	Laminated very fine light grey sandstone and dark grey shale: laminations very thin.	NOSSOB
236 - 238.5	2,5	Light grey very fine sandstone or siltstone.	
238.5 - 245	6,5	Sandy shale and shale.	
245 - 247	2	Shale, dark grey.	
247 - 249	2	Shale and mudstone with sandy shale with prominent drop-stones. Grey to dark grey.	DWYKA
249 – 250 EOH	1	Dark grey shale.	

Remarks:

1. This borehole was drilled by air-rotary method and mud-rotary only after grouting.

2

2. Only the Nossob horizons are screened.

This borehole was logged by F. Bockmuhl.

2. Penetration Record



	Penetration Recor		statement of the local division of the local	the second se
epth (m)	Pen. Rate (min/m)	Time	Date	Remarks
			28/7/00	Drilling air rotary
1				Water used for drilling 1400 micro S/cm
	1			
5				
	1.35			
	1.1			
	1.5			
10	2.3			
	1.5			
	1.45			
	1.45			
	1.45			
	1.66			
	2.2			
	2.25			
	2.3			
	2.85			
20				
	1.75			
	2.8			
	3.1			
	2.15			
	2.55			
	2.05	8		
	2.3			Water strike
	1.1			
	1.95			
30				
	3.85			
	3.9			
	1.85			
	1.35			
	3.8			
	3.1			
	2.25			
	2.95			
	1.8			
40				
	2.2			
	2.2			
	1.8			
	1.45			
	1.7			
	2.75			
	2.4			
	3.55			
	2.6			
50				
	4.75			
	1.85			

Sheet1

Page 1

	3.1			
	2.45			
	2.35			
	2.8			
	1.95			
	2.35			
	2.95			
60	4.45			
	3.3			
	2.55			Water sample: 1165 micro S/cm; 24.3 C
	6.2			
	2.25			
	2.95			
	2.95			
	3.95	40.40		4405
	0.05	16:18		1125 micro S/cm
70	3.85			
70	3.6			
	3.55			
	3.45			
	2.75			
	4.05			
	4.05			
	2.3			
	2.5			formation change
	7.3			
80	2.95			
	3.05			
	3.7			
	1.6			
	2.3			
	2			
	2.1			
	2.05			
	2.1			
	2.1			
90	2.2			
	2.15			
	1.85			
	1.25			
	1.95			
	2.35			
	2.05			
	2.2			
	2.8			
100	2.65			
100	2.05			End of 211 mm drilling
	6.45	12.15	30/07/00	End of 311 mm drilling.
	5.6	13.15	30/07/00	Start 254 mm drilling.Mud rotary Water used for drilling 1592 micro S/cm
	7.75			water used for unning 1592 micro S/Cm
	6.7	13:44		7.28 mS/cm
	6.6	10.44		7.20 110/011
	5.1			
	4.7	14:04		7.03 mS/cm

110	4.5			
110				
	3.45	44.04		5 00 mOlemental Free Min 401
	5.75	14:24		5.88 mS/cm add Eeze Mix 10 I
	5.9			
	6.35			5.17 mS/cm add 5 I Eeze Mix
	6.8			
	6.8	14:51		5.1 mS/cm
	7.15			
	7	15:11	30/07/00	4.63 mS/cm
100	7.15			
120	6.1			4.2 mS/cm
	66.6			
	3.5	08:08	31/07/00	Drilling with drag bit mud rotary
	3.4			
	3.2			
	2.45			
	2.5			1895 microS/cm 22.7 C
	2.7			
	8.2			1559 microS/cm 22.7 C add Ezee Mix
	16.15	08:42		Stop drilling with drag bit mud rotary
130	1.75	11:02	1/08/00	Drilling with tri-cone air rotary
	2.1			
	2.7			
	2.35			
	3.95			
	1.55			
	2.1			
	1.75			
	2.7			
	3.15			
140	3.2			
	3			
	3.3			
	3.55			
	3.15			Water strike ?
	2.9			
	2.55			
	2.35			
	2.1			
	3.25			
150	2.7			
	3.15			
	2.85			
	2.45			
	2.3			
	2.2			
	2.6			
	2.75			
	3			
	2.95			
160	1.9			
	3.45			
	3.35			
	3	13:37	1/8/00	Collect water sample for DWA & C-14
	3.4	0.000000000		

Sheet1

Page 3

	3.35			
	3.15			
	2.5			
	5.5			
	6.6			
170	8.75			
	6.15			
	5.65			
	4.95			
	5.25			
	5.7			
	4.75			
	5.35			
	5.4			
	4.8			
180	5.25			
100	5.5			
	8.5			
	5.6			
	3.25			
	3.3			
	3.75			
	4.1			
	3.4			
	3.25			
190	3.4			
	3.7			
	3.4			
	4.15			
	2.8			
	3.55			
	4.25			
	4.1			
	3.5			
	3.4			
200	3.85			
	3.6			
	3.8			
	3.8	17:30		
	6.2	17.00	3/08/00	Drilling 200 mm air rotary
	5.15		0,00,00	Shining 200 hinn all rotary
	5.6			
	6.4			
	5.5			
	6.45			
	3.9			
	4.5			
	4.4			
	4.4			
	4			
	4			
	4.6			
	3.7			
	3.6			
	3.55			
	4.1			

Sheet1

Page 4

6.5	
2.8	
3.2	
3.1	
2.9	
3.1	
3.15	
2.75	
6.9	
7.65	
7	
7.8	
6.25	
8.35	
4.6	
9.7	
18.15	
7.8	
4.1	
4.6	
4.5	
4	
4.45	
4.4	
2.6	
4.6	
5.35	
7.1	
7.55	

/	.00				
	6.7	17:35	3/08/00	End of Borehole.	



Penetration Record J 7 N

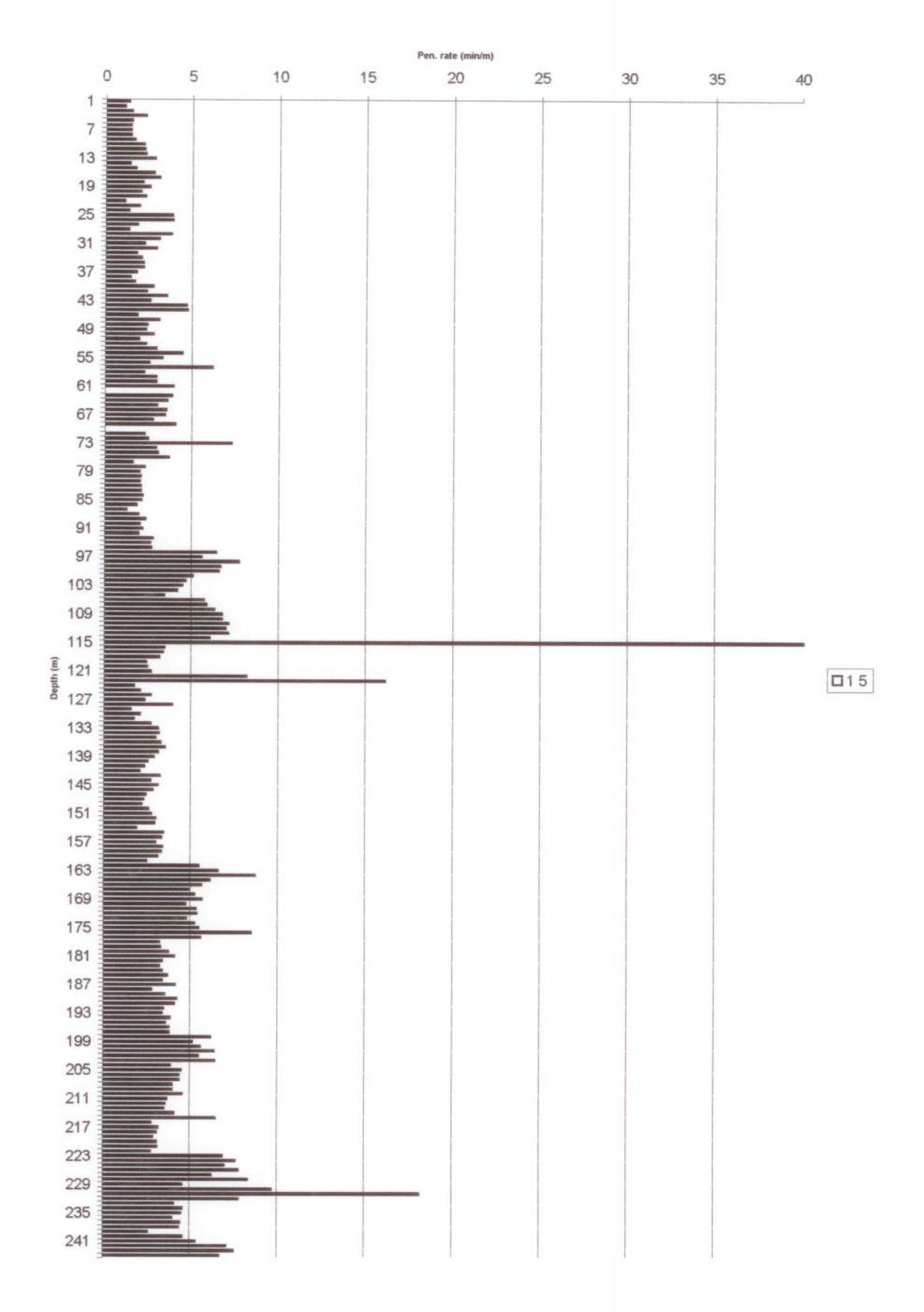


Chart2

3. Mud Rotary Drilling Log



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

MUD ROTARY DRILLING LOG

JICA REFERENCE: J 7 N LOCALITY: Jakkalsdraai R228 WW 39853

Remark: This borehole was drilled air-rotary with only for a short distance of mud-rotary employed.

TIME	DEPTH mbgl	MARSH FUNNEL TEST 1000 ml	MARSH FUNNEL TEST 500 ml	E. C. µS/cm	DENSITY	рН	TEMPERATURE ° C	COMMENT
(28/07/00)	62			1165			24.3	Represents water in borehole
16:18	68			1125				Collected sample
	101			1120			25.5	End of 311 mm drilling Represents conditions when logging.
				1400			16.5	Water + foam used for drilling
13:15 (30/07/00)	101			1592	<1.16		17.7	Water used for mixing drill- fluid when drilling mud- rotary.
13:44	105			728			24.3	
14:04	108			703			24.9	
14:35	114	39	27	517			25.7	
15:11	118			420			28.5	
08:27 (31/07/00)	126			1895			22.4	
08:42	129	38	27	1559			22.7	
11:02	130							Start drilling air-rotary

1

DATE: 28/07/00 (starting)

TIME	DEPTH mbgl	MARSH FUNNEL TEST 1000 ml	MARSH FUNNEL TEST 500 ml	E. C. µS/cm	DENSITY	рН	TEMPERATURE ° C
13:37				1363			27
17:30 (01/08/00)	203			1388			27.7
20:39 (03/08/00)	250			535 mS/m		10.6	27.8

COMMENT

Water with air

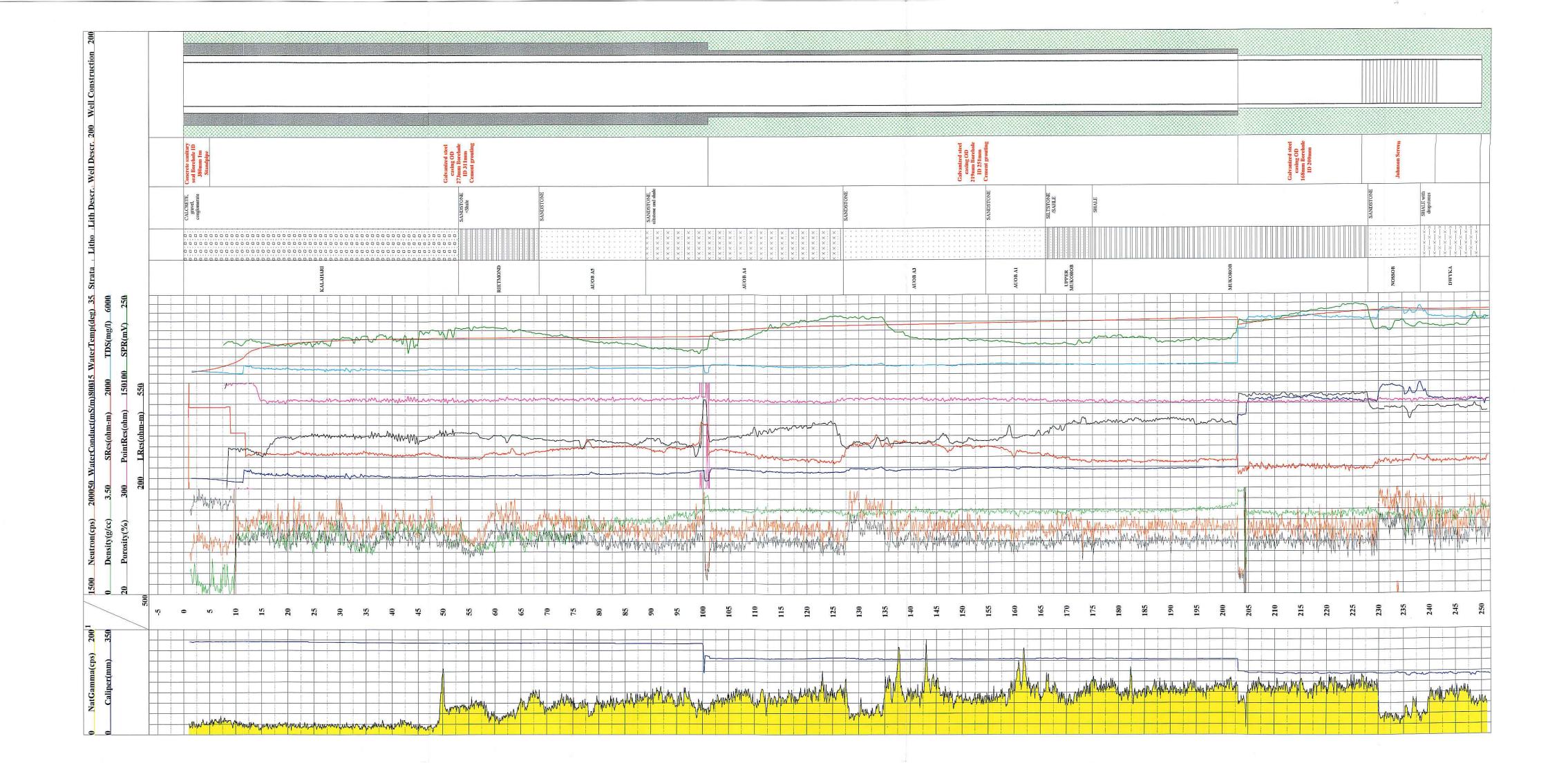
Water in borehole when logging. End of 250 mm drilling. Water in borehole when

logging. End of drilling.

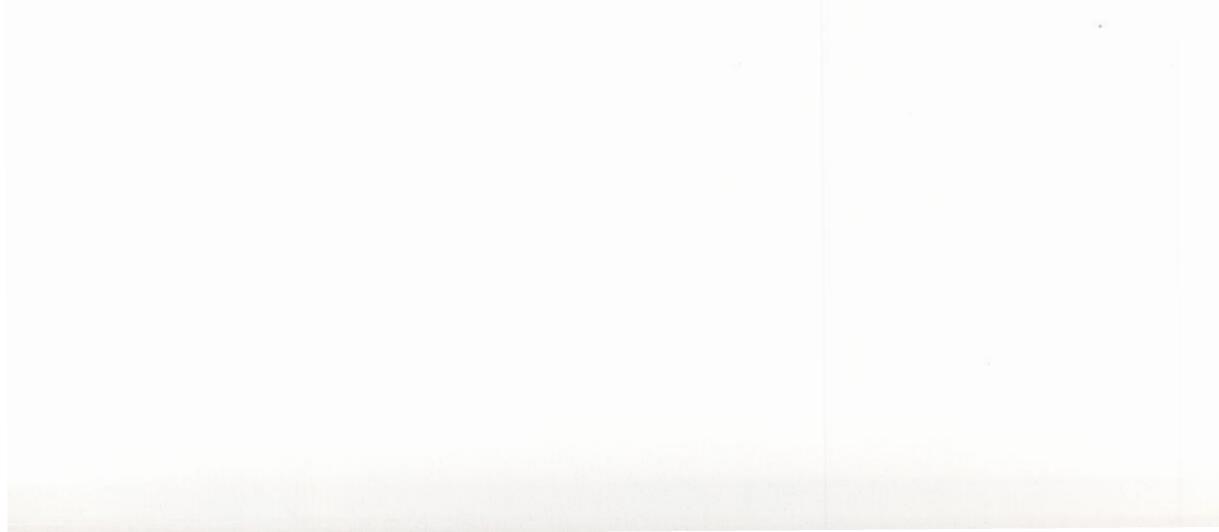
4. Geophysical Log and Casing Design



Pos	eiden Geophysics (Pey. No. 537550)				
	CONSULTANT PACIFIC CONSULTANTS INTERNATIONAL				
	COMPANY METZGER PM DRILLING				
1	PROJECT The Study on the Groundwater Potential Evaluation and Management Plan in the Southeast Kalahari (Stampriet) Artesian Basin				
Si a	WELL ID J7N WW39853				
WW bala	LOCATION JAKKALSDRAAI				
CO. Pose WELLJ7N PROJ. LCN. Jaki STE. J 7 FILING No.	COUNTRY REPUBLIC OF NAMIBIA				
3H COORDINATES					
COLLAR ELEVATION LOG MEAS. FROM Gr	oundlevel				
DRILLING MEAS. FROM	1 Groundlevel				
DATE 4 August 2000					
YPE LOG Physical Properties					
EPTH-DRILLER 250m EPTH-LOGGER 251.8m					
TM LOGGED INTERV					
OP LOGGED INTERVA					
ERMANENT DATUM	Groundlevel				
RECORDED BY	Wimpie Coetzer				
WITNESSED BY	Frank Bokmuhl				
	JAPAN INTERNATIONAL COOPERATION AGENCY				



5. Borehole Development Data



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

BOREHOLE DEVELOPMENT DATA

JICA REFERENCE: J 7 N

LOCALITY: Jakkalsdraai R 228

WW 39853

TIME (actual)	P.I.D. (mbsu)	½ 90° V- Notch (mm)	Yield (m ³ /h)	E.C. (mS/m)	Water Level (mobs)	Remarks
14:00	227	80		436	27.30	Date 7/08/2000
16:00		26		627	34.27	
20:00		25			39.40	Pump through the night
07:00	227	20				Date 8/08/2000. Add 1 pipe
08:00	233	40		807	62.28	
12:00		25			66.72	
16:00		35			68.20	
19:00		25			69.36	Pump through the night.
07:00					70.55	Date 9/8/00. Add 2 pipes. Water level measured just before the start of the next airlift session.
08:00	245	25			70.36	
12:00		20			77.54	
16:00		20			82.55	
19:00		20		428	84.30	Pump through the night.
07:00						Date 10/08/2000: Development stopped.

Remarks:

- 1. Date 6/8/2000: 25 kg of polyphosphates (introduced into borehole already on 5/8/00) were re-circulated for a total of 11 hours by means of air lift as part of the development.
- 2. This low yielding borehole was also pumped by electrical submersible pump as part of the development. After 2.35 hours this was abandoned and it was decided to do a short pumping test.

DATE: 6/08/2000 (starting)

6. Evaluation of Pumping Test



1. PUMPING TEST ANALYSIS

J7-N (WW39853) - Pumping well

1.1. Well Efficiency (Step draw down test) (Annex 1)

Well Efficiency was analysed by making use of the Jacob method for draw down data. Aquifer parameters used for the calculation of well efficiency were obtained from the evaluation results of the constant discharge test, which is discussed in **Section 1.2** below.

The well efficiencies at the range of pumping rates used during the step draw down test are summarised in **Table 1** below. Only four of the two steps were utilised for the evaluation of the borehole efficiency. The third step was interrupted due to pumping problems caused by accumulation of gas in the pump. The well bore effect is dominant throughout the test and only the last 10 minutes of each 120 minutes step was used for the evaluation.

Borehole number	Step	Abstraction Rate [m ³ /h]	Draw Down* [m]	Borehole Efficiency [%]
J7-N	1	0.3	18.1	86.6
	2	0.6	45.2	69.3

Table 1: J7-N; Borehole efficiency at various pumping rates

* at cut-off time Δt , after which well bore storage has no affect on the well performance

Data on the linear and non-linear well losses and skin factors as well as the efficient well radius are presented in Annex 1.

1.2. Constant Discharge Test Analysis (Annex 2 - 3)

The constant discharge draw down curve of abstraction borehole **J7-N** indicates leakage. For leaky aquifers, the Walton Hantush analysis method with draw down and recovery data was once again used to calculate the hydraulic conductivity of the aquifer and the aquitard **(Annex 2 & 3)**.

Aquifer storativity was estimated due to the fact that no suitable observation boreholes was available. The constant discharge test was implemented at a rate of 0.3 m³/h and was stopped after 9 hours, due to a draw down of 66 m. The water level was close to pump inlet depth. The water level recovered fully after three days. The recovery curve was evaluated using the Theis recovery method.

The results of the constant discharge analysis are summarised in **Table 2** below. The transmissivity of the test pumping is compared to the results of the slug test. Again, the transmissivity of the slug test is slightly higher, due to the bigger influence of the gravel pack and the disrupted formation surrounding the borehole. The evaluated very low values of T = 0.01 and $0.06 \text{ m}^2/\text{day}$ are, however, in the same order of magnitude.

1

Borehole number	Analysis Method	Т	S	k	S	Simulation mode
		[m ² /day]	[m]	[cm/sec]	[-]	Simulation mode
J7-N	Theis recovery	0.01	17	6.8 x 10 ⁻⁷	*8 x 10 ⁻⁴	Theis
	Slug test (for comparison)	0.06	17	2.1 x 10 ⁻⁶	N/A	Cooper et al

Table 2: Aquifer Parameters calculated for J7-N; Nossob sandstone

*Estimated

The Theis model for confined aquifer conditions was used to simulate and verify the actual data and analysis approach of the constant discharge test. Simulation parameters summarised in **Table 2** were used in simulation of the actual pumping test data (See **Annex 3** for simulation results).

The radius of influence (R) was estimated after SICHARDT (1928) using the equation:

 $R = 3000 \times s \times K_f^{1/2}$

 $R = 3000 \times 66.61 \times 8.3 \times 10^{-5} = 17 \text{ m}$

where

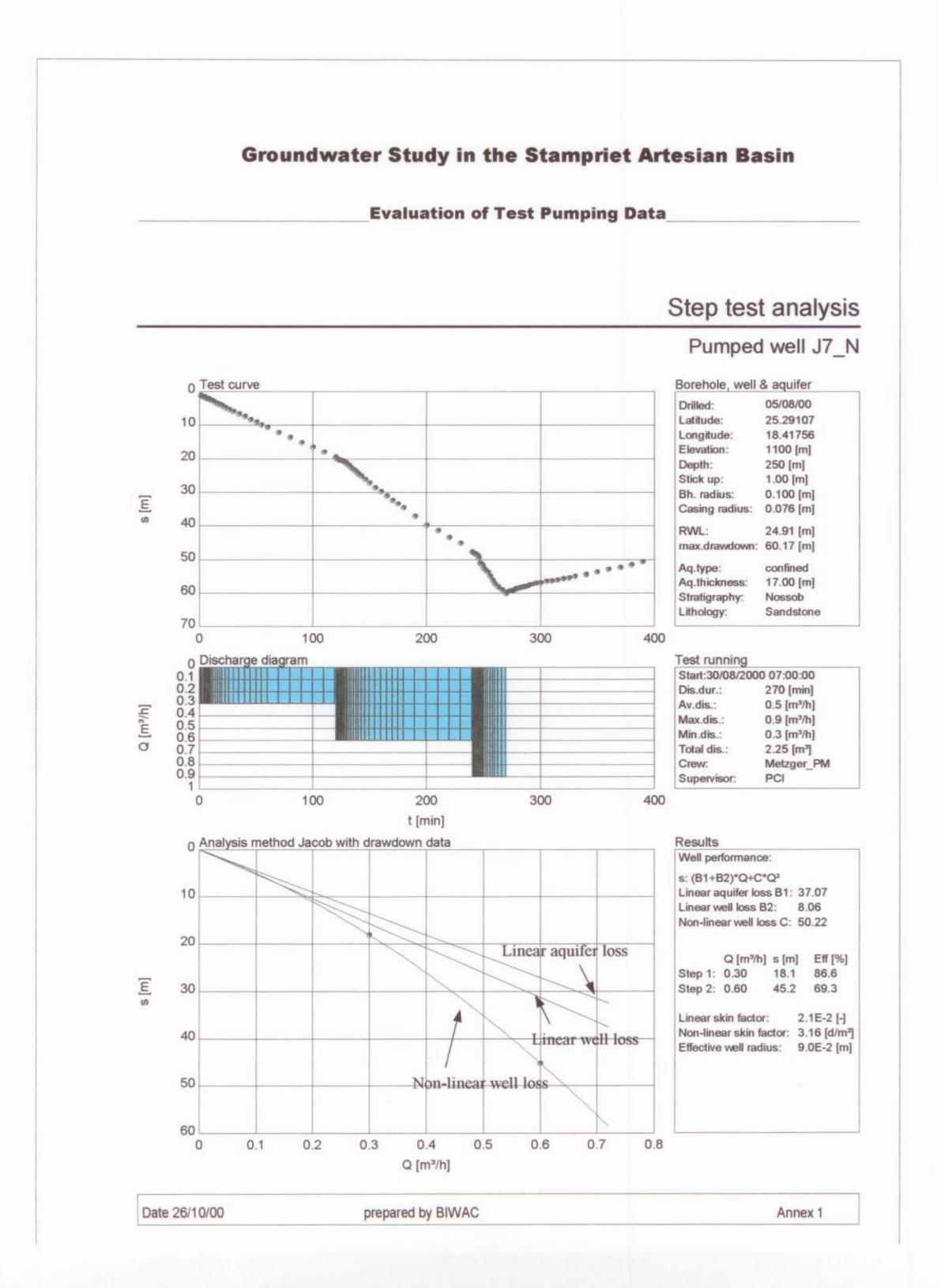
R = Radius of influence

s = Draw down in abstraction borehole at end of pumping

K_f = Permeability of the aquifer

The equation is approximately correct for unconfined aquifers. In case of a confined aquifer the radius of influence most probably larger and the 17 m are considered to be the minimum value.

A proper evaluation of R (and storativity S) will only be possible once reliable data from observation wells, penetrating the same aquifer as the pumped well, are available.

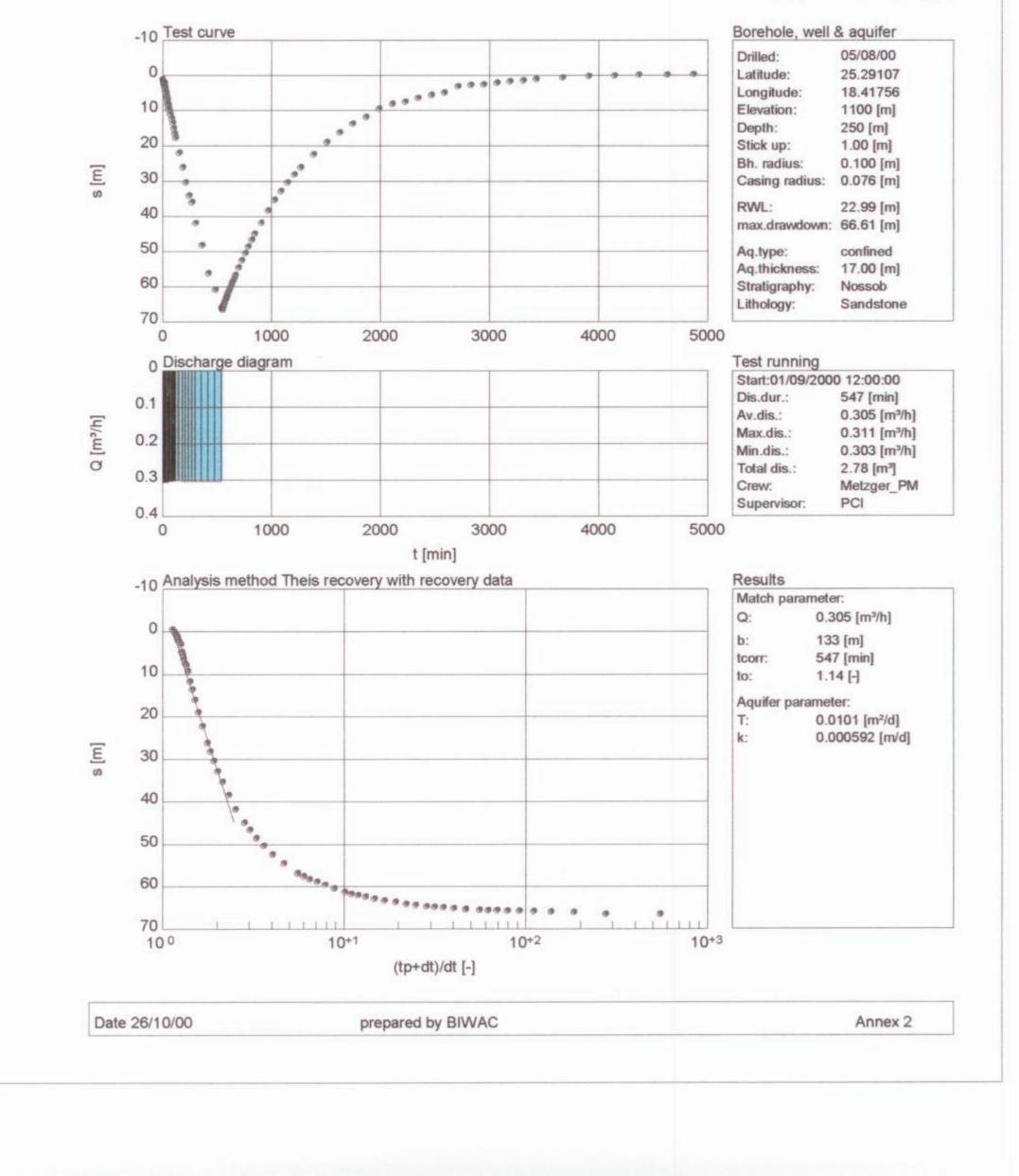


Groundwater Study in the Stampriet Artesian Basin

Evaluation of Test Pumping Data

Test pumping analysis

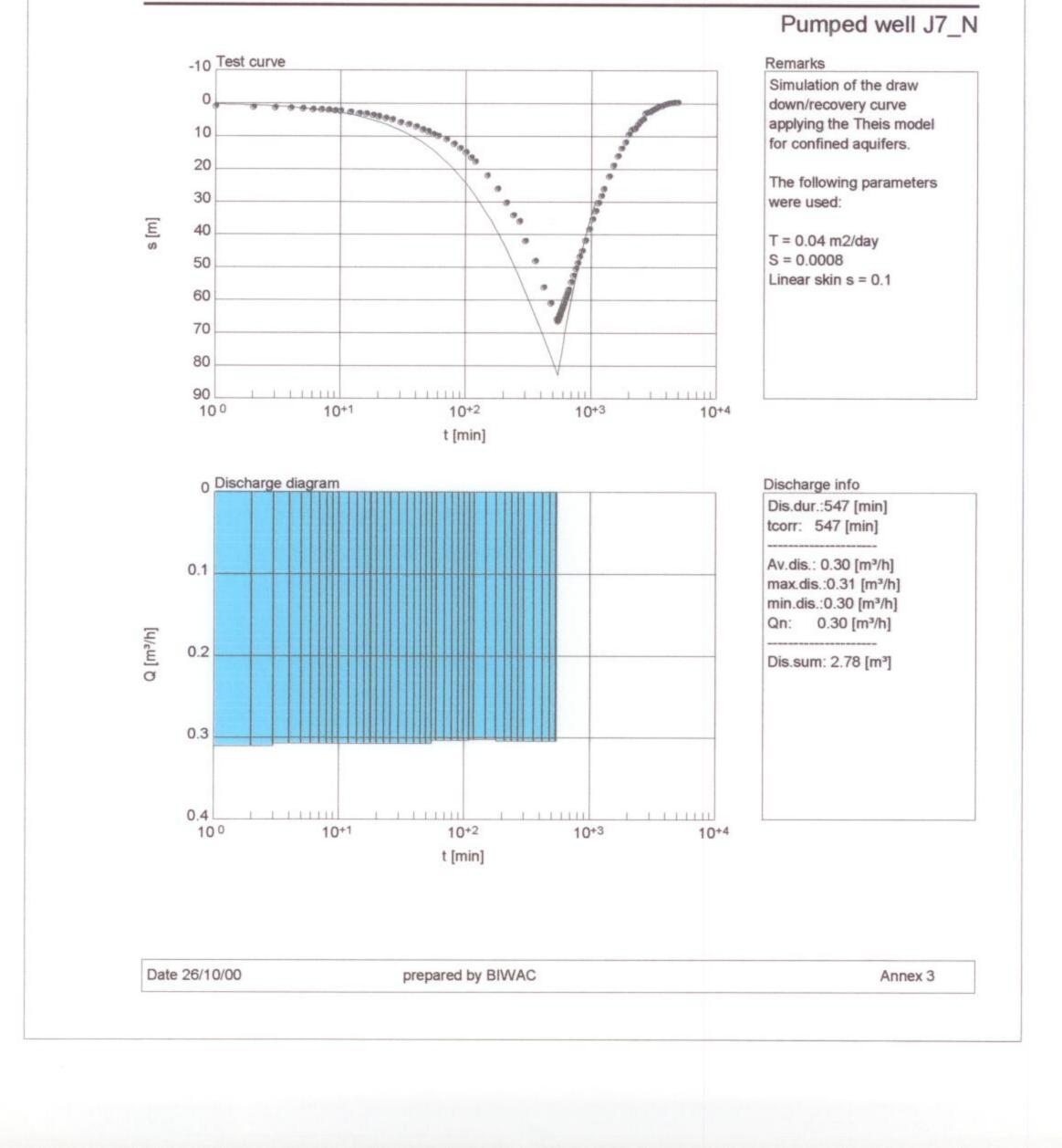
Pumped well J7_N



Groundwater Study in the Stampriet Artesian Basin

Evaluation of Test Pumping Data

Step test diagnosis



STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN FOR THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN IN THE REPUBLIC OF NAMIBIA

Japan International Co-operation Agency JICA Study Team

EVALUATION OF TEST PUMPING DATA

Borehole J6-A (WW39850) Cobra



METZGER PM DRILLING Box11733

Windhoek

Namibia

Windhoek

August 2000

7. Water Level Recorder Installation



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

INSTALLATION OF SEBA FLOATERS

JICA REFERENCE: J 7 N LOCALITY: Jakkalsdraai R228

WW 39853

1.	Serial Number of floater:	4552
2.	Date installed:	5/10/00
3.	Rest Water Level when installed:	23.01 mbsu
4.	Distance from stick-up to logger:	18.00
5.	Distance from logger to water level:	5.01
6.	Cut off:	18.0 (0.91 + 17.11)

