STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN FOR THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN IN THE REPUBLIC OF NAMIBIA

Japan International Cooperation Agency Pacific Consultants International

BOREHOLE FINAL REPORT

Borehole J8-K (WW 39854) Twee Reviere R481

METZGER PM DRILLING

P.O.Box 11733 Windhoek Namibia

> Windhoek October 2000



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1. Geological Borehole Log



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

| Farm Twee Reviere | WW 39854 | | |
|--------------------------------|----------------------|--|--|
| Jica Reference: J 8 K | S 25.46122° | | |
| Date completed: 21 / 07 / 2000 | E 19.43266° | | |
| | Collar elev.: 1015 m | | |

| GEOL | OGI | CAL | BOREHOLE LOG | |
|-------|------|-----|---------------------|--|
| OL OL | 1001 | ~ | DOILDITOLL LOO | |

| Depth below surface (m) | Section (m) | Lithology | Stratigraphy |
|----------------------------|----------------|---|--------------|
| 0 - 3 | 3 | Calcrete, moderately karsted. Shallow cover of pale orange sand. Karst cavities filled with orange to pale red sand. | |
| 3 - 12 | 9 | Pinkish calcretized conglomerate . Matrix is a fine to medium grained pinkish grey calcareous sandstone, with pebbles and boulders of grey and brown quartzite and sandstone. | |
| 12 - 14 | 2 | Very light grey to white sandy calcrete. | KALAHARI |
| 14 - 19 | 5 | Pale grey to pale brown sandy calcrete . Drill-cuttings recovered in a clayey mass. Saline encrustations on dry cuttings. (= sulphate ?) | |
| 19 - 30 | 11 | Pale grey to white sandy calcrete with minor clayey horizons at 23 & 28 m. At 21 m red sandstone pebbles in calcareous sandstone matrix. | |
| 30 - 36 | 6 | Sandstone very pale brown, mostly fine grained unsorted, calcareous. Grains sub-rounded. Saline coating on dry drill cuttings. | |
| 36 – 129 EOH | 105 | Sandstone, generally pale reddish brown, gradually changing to reddish brown at depth. Grain-size unsorted, very fine to medium, and generally finer grained at 135 to 141 m. Aquifer (saline!) Collected drill cuttings when dried before washing all develope a white saline coating | |

REMARKS:

- 1. Screens from 84,60 m to 96,30 m and from 102.30 m to 114.0 m.
- 2. Gravel emplaced up to 12 m from ground level. Total length of gravelpack is 117 m.

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3. This borehole was drilled by the mud-rotary method, resulting in a highly ground mass of drill-cuttings, which have to be carefully washed and interpreted.

This borehole was logged by F. Bockmuhl.

2. Penetration Record



j8kpen

| | Penetration Record | d Borehole | J8K WW 3 | 9854 | |
|-----------|---|------------|--------------|---------------------------|---|
| Depth (m) | Pen. Rate (min/m) | Time | Date | Remarks | |
| 1 | and the second second second second second second | Time 12:30 | Date 16/7/00 | Drilling Air rotary 311mm | |
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| 10 | | | | | |
| | 1.05 | | | | |
| | 1.8 | | | | |
| | 2.1 | | | | |
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| | 2.25 | | | | |
| | 2.05 | | | | |
| | 1.8 | | | | |
| | 2.2 | | | | |
| | | | | | |
| 20 | | | | | |
| | 2.6 | | | | |
| | 3.25 | | | | |
| | 2.15 | Time 14:24 | | | |
| | 2.45 | | | | |
| | 2.25 | | | | |
| | 2.5 | | | | |
| | 2.7 | | | | |
| | 2.85 | | | | |
| | 1.4 | | | | |
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| 40 | 2.25 | | | | (|
| | 2.1 | | | | |
| | 2.85 | | | | |
| | 2.3 | Time 15:25 | | | |
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| | 2 | | | | |
| | 1.75 | | | | |
| 50 | 2.7 | | | | |
| | 1.65 | | | | |
| | 1.6 | | | | |
| | 1.5 | | | | |

Sheet1

Page 1

j8kpen

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| | 1.05 | | | |
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| 70 | 1.25 | | | - |
| | 1.35 | | | |
| | 1.55 | | | |
| | 1.3 | | | |
| | 1.65 | | | |
| | 2.3 | | | |
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| | 2.45 | Time 16:47 | | |
| | 2 | | | |
| 80 | 1.6 | | | |
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| | 0.9 | | | |
| | 0.95 | | | |
| | 1.25 | | | |
| 100 | 1.25 | | | |
| 100 | 1.4 | | | |
| | 0.85 | | | |
| | 0.95 | | | |
| | 1.7 | | | |
| | 1.45 | | | |
| | 1.3 | | | |
| | 1.45 | | | |
| | 1.7 | | | |
| | 1.4 | | | |
| | 1.6 | | | |

Sheet1

Page 2

| 110 | 1.5 | | | |
|-----|------|--|-----------------|--|
| | 1.5 | | | |
| | 1.7 | | | |
| | 1.7 | | | |
| | 1.1 | | | |
| | 1.4 | | | |
| | 1.55 | | | |
| | 1.55 | | | |
| | 1.3 | | | |
| | 1.85 | | | |
| 120 | 1.95 | | | |
| | 1.55 | | | |
| | 1.5 | | | |
| | 0.9 | | | |
| | 0.9 | | | |
| | 1.1 | | | |
| | 1.4 | | | |
| | 0.75 | | | |
| | 0.6 | | End of borehole | |



j8kpen



Penetration Record J 8 K

Pen. Rate (min/m)



Chart2

3. Mud Rotary Drilling Log



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

MUD ROTARY DRILLING LOG

JICA REFERENCE: J 8 K LOCALITY: Twee Reviere R 481 WW 39854 DATE: 17/07/00

| TIME | DEPTH mbgl | MARSH FUNNEL TEST 1000 ml (sec) | MARSH FUNNEL TEST 500 ml (sec) | E. C. mS/cm | DENSITY | рН | TEMPERATURE ° C | |
|-------|---------------|---------------------------------------|--------------------------------------|----------------|---------|----|--------------------|--|
| 16:47 | 78 | 28 | | 7,25 | | 9 | 21 | |
| 18:25 | 128 | 29 | | 4,69 | | 9 | 23 | |

This borehole was drilled by air rotary method, as better drill cuttings could be obtained.

COMMENT

Water used for air rotary drilling. This borehole was drilled air rotary and filled with drillfluid as recorded.

4. Geophysical Log and Casing Design



| Second State Stat | 2051 | eiden Geophysics (Rog. No. 037550) |
|--|--|---|
| Section of the section of the section of the Groundwater Potential Evaluation and Management Plan in the Southeast Kalahari (Stampriet) Artesian Basin WELL ID J8K WW39854 LOCATION TWEE RIVIERE OUNTRY REPUBLIC OF NAMIBIA OUNTRY REPUBLIC OF NAMIBIA SHI COORDINATES COLLAR ELEVATION COMEAS. FROM Groundlevel DRILLING MEAS. FROM GROUNDL DRIVENT DATUM Groundlevel DRIVENT DATUM Groundlevel DRIVENT DATUM Groundlevel DRIVENT DATUM Groundlevel DRIVENT DATUM GROUNDL DRIVENT DATUM GROUNDL DRIVENT DATUM GROUNDL DRIVENT DATUM GROUNDL | | CONSULTANT PACIFIC CONSULTANTS INTERNATIONAL |
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5. Borehole Development Data



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

BOREHOLE DEVELOPMENT DATA

JICA REFERENCE: J 8 K LOCALITY: Twee Reviere R 481 WW 39854 DATE: 22/07/2000 (starting)

| | Water Level (mbsu) | E.C. (mS/m) | Yield (m ³ /h) | ½ 90° V- Notch (mm) | P.I.D. (mbsu) | TIME (actual) |
|--------------------|-----------------------|----------------|------------------------------|---------------------------|------------------|------------------|
| Date 22/07/00. Cal | | | | | | 10:00 |
| Date 23/07/00. Pl | 41 | | | | | 08:00 |
| Date 24/07/00. p | 56.4 | 546 | | | | 08:00 |
| Date 25/07/00. I | 60.80 | 480 | | | | 12:00 |
| Date 26/07/ | 60,60 | | | | | 08:00 |
| Date | | | | | 83 | 09:45 |
| | 63.32 | | | | | 10:00 |
| | 63.24 | | 0.25 | 25 | | 11:00 |
| | 73.36 | | | 25 | | 12:00 |
| | 74.50 | | | 25 | | 13:00 |
| | 87.40 | | 2.16 | 60 | 95 | 14:00 |
| | 87.42 | | 0.36 | 30 | | 15:00 |
| | 87.55 | | | 28 | | 16:00 |
| Pump | 87.44 | | 0.25 | 25 | | 16:30 |
| D | 69.34 | | 0.36 | 30 | 107 | 09:00 |
| | 74.42 | | | 35 | | 10:00 |
| | 74.43 | | | 30 | | 11:00 |
| | 75.44 | | | 30 | | 12:00 |
| | 79.44 | | 0.25 | 25 | | 16:00 |
| | 82.54 | | | 28 | | 17:00 |

| Remarks |
|--------------------------------|
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| |
| ole Tool. Plunging for 7 hours |
| inge for 8 hours, bail 1 hour. |
| lunge 5 hours, bail 4 hours. |
| lunge 1 hour, bail 3 hours. |
| 00. Bailing for 9 hours. |
| 28/07/00: Airlift |
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| hrough the night. |
| te 29/07/00. |
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| TIME (actual) | P.I.D. (mbsu) | ½ 90° V- Notch (mm) | Yield (m ³ /h) | E.C. (mS/m) | Water Level (mbsu) | Remarks |
|------------------|------------------|---------------------------|------------------------------|----------------|-----------------------|---------------------------|
| 19:00 | 107 | 28 | 0.3 | | 84.31 | Pump through the night. |
| 07:00 | | | | | | Date 30/07/00. Add pipes. |
| 10:00 | 116 | 60 | | | 74.36 | |
| 11:00 | | 40 | | | 75.56 | |
| 16:00 | | 30 | 0.36 | | 78.52 | |
| 19:00 | | 28 | | | 78.42 | Pump through the night. |
| 07:00 | | 25 | | | 82.43 | |
| 09:00 | 116 | 30 | 0.36 | | 83.36 | Stop airlift. |

Remarks:

1. This borehole was also developed by electrical submersible pump on 9/8/00. Data captured below.

| TIME (actual) | Pump time (min) | Water Level (mbsu) | Yield (m ³ /h) | E.C. (mS/m) |] |
|------------------|-----------------------|-----------------------|---------------------------|----------------|---|
| 07:01 | 1 | 81.10 | | | |
| | 2 | 83.74 | | | |
| | 3 | 82.30 | | | |
| | 4 | 80.24 | | | |
| | 5 | 79.28 | | | |
| | 6 | 78.10 | | | |
| | 7 | 78.05 | | | |
| | 8 | 77.40 | | | |
| | 9 | 77.62 | | | |
| | 10 | 77.85 | 1.029 | | |

| Remarks | | |
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| Remarks | |
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| TIME (actual) | Pump time (min) | Water Level (mbsu) | Yield (m ³ /h) | E.C. (mS/m) | 1 |
|------------------|-----------------------|-----------------------|---------------------------|----------------|---------------|
| | 205 | | 0.213 | | |
| | 210 | 103.78 | 0.209 | | |
| | 215 | | | | |
| | 220 | 102.84 | | | |
| | 230 | | 0.195 | | |
| | 240 | 100.02 | 0.301 | | Ope |
| | 250 | | | | |
| | 260 | 99.35 | | | |
| | 270 | 98.95 | | | |
| | 280 | 98.48 | | | |
| | 300 | | 0.307 | | |
| | 320 | 97.29 | | 463 | |
| | 340 | | | | |
| | 360 | 96.13 | | | |
| | 380 | | | | |
| | 400 | 95.24 | 0.310 | | |
| | 420 | 94.82 | | | |
| | 440 | | | | |
| | 460 | 94.26 | | | |
| | 480 | | 0.317 | | |
| | 500 | 93.73 | | | |
| | 520 | | | 405 | |
| 16:00 | 540 | 93.41 | 0.320 | | Stop developi |
| 16:18 | | 91.24 | | | |

| Remarks |
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| ng. Measure recovery. |
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6. Evaluation of Pumping Test



1. PUMPING TEST ANALYSIS

J8-K (WW39854) - Pumping well

J8-A (WW39855) - Observation well

J8-N (WW39856) - Observation well

1.1. Well Efficiency (Step Drawdown Test) (Annex 1)

Well Efficiency could not be evaluated due to the very low abstraction rates and minimal differences of the individual steps. The step draw down curve is presented in Annex 1.

The abstraction rates and respective draw down are summarised in Table 1 below.

| Borehole number | Step | Abstraction Rate [m ³ /h] | Draw Down* [m] |
|--------------------|------|---|-------------------|
| J6-K | 1 | 0.1 | 2.98 |
| | 2 | 0.2 | 6.07 |
| | 3 | 0.3 | 11.54 |
| | 4 | 0.4 | 19.65 |
| | 5 | 0.5 | 31.79 |

Table 1: J8-K: Borehole efficiency at various pumping rates

* at cut-off time Δt , after which well bore storage has no affect on the well performance

1.2. Constant Discharge Test Analysis (Annex 2 - 4)

The abstraction rate of the constant discharge test was <u>0.25 m³/h</u>. The constant discharge draw down curve of abstraction borehole **J8-K** and the Lithology indicate unconfined phreatic conditions. However, confined conditions cannot be excluded. The Theis method with draw down and recovery data was used to calculate the hydraulic conductivity of the aquifer **(Annex 2 & 3)**.

The rapid recovery to levels higher than the original rest water level could be an indication for clogging and ongoing borehole development during pump testing. In case of confined conditions this behaviour could be attributed to changes in atmospheric pressure.

At very low abstraction rates the standard pumping test evaluation becomes somewhat unreliable and the results should be compared with the results from the proposed slug test.

The aquifer storativity had to be estimated due to the fact that the observation boreholes **J8-A** and **J8-N** do not penetrate the same aquifer as **J8-K**. During the duration of the constant discharge test, a rise in the water levels of observation boreholes **J8-A** and **J8-N** is observed. (See Annex 4).

1

The results of the constant discharge analysis are summarised in Table 2 below.

Table 2: Aquifer Parameters calculated for J8-K; Kalahari

| Borehole number | Analysis method | т | s | k | S | | |
|--------------------|---------------------|----------|--------------|------------------------|-----------------------|---|--|
| | | [m²/day] | [m] [cm/sec] | | [-] | Comments | |
| 10 1/ | Theis- draw down | 0.132 | 30 | 5.1 x 10 ⁻⁶ | *5 x 10 ⁻³ | *Storativity estimated - Observation boreholes are not located in the tested aquifer | |
| J8-K | Theis- recovery | 0.122 | 30 | 4.7 x 10 ⁻⁶ | *5 x 10 ⁻³ | | |

The Phreatic as well as the confined model was used to simulate and verify the actual data and analysis approach of the constant discharge test.

The radius of influence (R) was estimated after SICHARDT (1928) using the equation:

 $R = 3000 \times s \times K_f^{1/2}$

 $R = 3000 \times 17.3 \times 2.2 \times 10^{-4} = 12 m$

where

R = Radius of influence

s = Draw down in abstraction borehole at end of pumping

K_f = Permeability of the aquifer

The equation is approximately correct for unconfined aquifers. The 12 m are considered to be the minimum value. The distance of the observation boreholes is, however, far beyond the radius of influence (J8-A = 121.7m and J8-N = 61.4 m).

A proper evaluation of R (and storativity S) will only be possible once reliable data from observation wells, penetrating the same aquifer as the pumped well, are available.





Groundwater Study in the Stampriet Artesian Basin

Evaluation of Test Pumping Data

Test pumping analysis

Pumped well J8_K



Groundwater Study in the Stampriet Artesian Basin

Evaluation of Test Pumping Data

Test pumping analysis

Pumped well J8_K



Groundwater Study in the Stampriet Artesian Basin

Evaluation of Test Pumping Data

Test pumping diagnosis



Pumped well J8_K

1. EVALUATION OF SLUG TEST

Borehole J8-K was tested using a 3 m long slug. The first test was done after the slug was lowered (See Figures 1 and 2), while the second test was done after the slug was pulled out of the borehole (See Figures 3 and 4).

The Cooper Bredenhoeft-Papadopulos (type curve) and Bouwer-Rice (straight line) solutions for confined aquifers were used to evaluate the transmissivity and hydraulic conductivity of the aquifer (See Table 1). Borehole J8-K was also pump tested and the results of the Theis draw down and recovery solutions were 0.132 m²/day and 0.122 m²/day respectively.

| Test | Solution | T [m²/day] | K [cm/sec] | Y₀ [m] | S* [] |
|----------------------------------|-------------------------------|---------------|------------------------|-----------|-------------------------|
| Lower Slug | Cooper-Bredehoeft-Papadopulos | 0.27 | | | 1.6 x 10 ⁻¹⁰ |
| | Bouwer-Rice | | 7.1 x 10 ⁻⁶ | 1.06 | |
| Pull Slug | Cooper-Bredehoeft-Papadopulos | 0.31 | | | 1.0 x 10 ⁻¹⁰ |
| | Bouwer-Rice | | 8.3 x 10 ⁻⁶ | 1.00 | |
| Pumping test (for comparison) | Theis draw down | 0.132 | | | |
| Pumping test (for comparison) | Theis recovery | 0.122 | | | |

Table 1: Solutions for slug test J8-K (confined Kalahari aquifer)

* estimated

T = transmissivity [m²/day]

K = hydraulic conductivity [cm/sec]

- Y₀ = original displacement [m]
- S* = estimated storativity [--]





Figure 1: Lower slug; Cooper-Bredehoeft-Papadopulos Solution



Figure 2: Lower slug; Bouwer-Rice Solution

2



Figure 3: Pull slug; Cooper-Bredehoeft-Papadopulos Solution



3

Figure 4: Pull slug; Bouwer-Rice Solution

7. Water Level Recorder Installation



THE STUDY ON THE GROUNDWATER POTENTIAL EVALUATION AND MANAGEMENT PLAN IN THE SOUTHEAST KALAHARI (STAMPRIET) ARTESIAN BASIN

INSTALLATION OF SEBA FLOATERS

JICA REFERENCE: J 8 K LOCALITY: Twee Reviere R 481

WW 39854

| 1. | Serial Number of floater: | 4548 |
|----|--------------------------------------|-----------------------|
| 2. | Date installed: | 04/10/00 |
| 3. | Rest Water Level when installed: | 61.06 mbsu |
| 4. | Distance from stick-up to logger: | 55.0 m |
| 5. | Distance from logger to water level: | 6.06 m |
| 6. | Cut off: | 55.0 m (0.91 + 54.11) |

